

UCH 42 Triode-hexode frequency changer

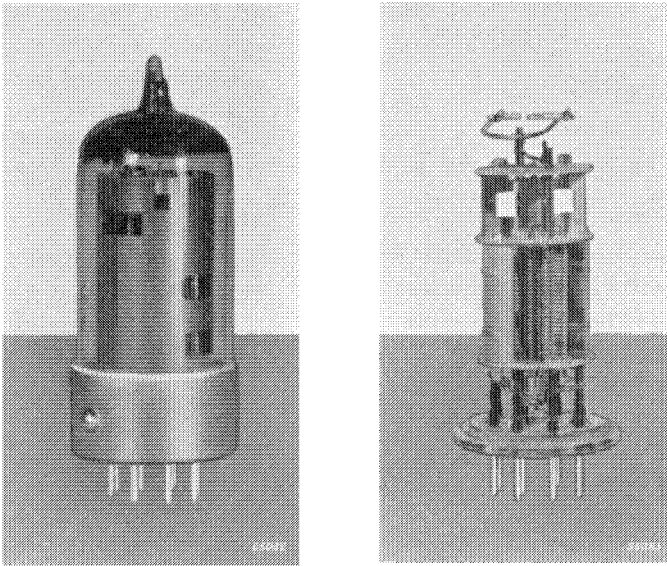


Fig. 1
The UCH 42, showing the electrode system (approximately actual size).

The triode-hexode UCH 42 is a frequency changer with a conversion conductance of $670 \mu\text{A/V}$ at an applied voltage of 170 V, or $530 \mu\text{A/V}$ at 100 V. It is designed for A.C./D.C. receivers in which the heaters, connected in series, take a current of 100 mA.

Further particulars will be found in the description of the ECH 42, the corresponding E-type valve.

TECHNICAL DATA OF THE TRIODE-HEXODE UCH 42

Heater data

Heating : indirect, A.C. or D.C., series feed

| | | | |
|--------------------------|-------|---|--------|
| Heater current | I_f | = | 100 mA |
| Heater voltage | V_f | = | 14 V |

Capacitances (measured on cold valve)

Hexode section

| | | | |
|---------------------------------|-----------|---|---------|
| Input capacitance | C_{g1} | = | 4.0 pF |
| Output capacitance | C_a | = | 9.4 pF |
| Anode - control grid | C_{ag1} | < | 0.1 pF |
| Heater - control grid | C_{g1f} | < | 0.15 pF |

UCH 42

Triode section

| | | | |
|------------------------------|----------------|---|--------|
| Input capacitance | C_{gT+g3} | = | 5.9 pF |
| Output capacitance | C_a | = | 2.4 pF |
| Anode - grid | $C_{(gT+g3)a}$ | = | 1.3 pF |

Between triode and hexode sections

| | | | |
|---|-------------------|---|---------|
| Hexode control grid - triode grid | $C_{g1H-(gT+g3)}$ | < | 0.35 pF |
| Hexode anode - triode grid | $C_{aH-(gT+g3)}$ | < | 0.2 pF |

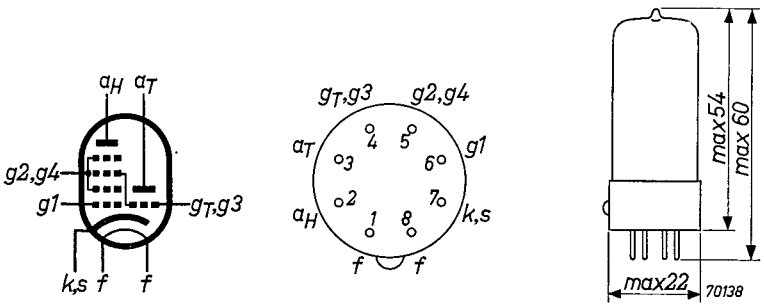


Fig. 2
Electrode arrangement, electrode connections and maximum dimensions in mm of the UCH 42.

Operating characteristics of the hexode section used as frequency changer (screen grids fed by means of a potentiometer, see Figs. 6 to 15 incl.)

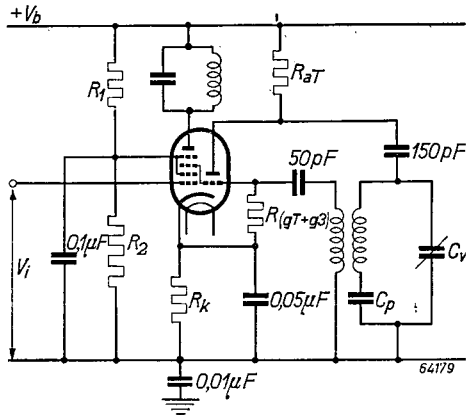


Fig. 3

| | | | | |
|--|---------------|-------------------|-------------------|-------------------|
| Anode and supply voltage | $V_a = V_b =$ | 100 | 170 | V |
| Resistor between supply voltage and screen grids | $R_1 =$ | 18 | 18 | k Ω |
| Resistor between screen grids and chassis | $R_2 =$ | 27 | 27 | k Ω |
| Bias resistor | $R_b =$ | 180 | 180 | Ω |
| Oscillator grid leak | $R_{gT+g3} =$ | 22 | 22 | k Ω |
| Oscillator grid current | $I_{gT+g3} =$ | 175 ¹⁾ | 350 ¹⁾ | μ A |
| Grid bias | $V_{g1} =$ | -1.0 — 13.5 | -1.85 — 25 | V |
| Screen grid voltage | $V_{g2+g4} =$ | 43 | 57 | 70 100 V |
| Anode current | $I_a =$ | 1.2 | — | 2.1 — mA |
| Screen grid current | $I_{g2+g4} =$ | 1.46 | — | 2.6 — mA |
| Conversion conductance | $S_c =$ | 530 | 5.3 | 670 6.7 μ A/V |
| Internal resistance | $R_i =$ | >1 | >5 | >1 >5 M Ω |
| Equivalent noise resistance | $R_{eq} =$ | 50 | — | 85 — k Ω |

| | | | | |
|--|---------------|--|-------------------|---------------|
| Anode and supply voltage | $V_a = V_b =$ | | 200 | V |
| Resistor between supply voltage and screen grids | $R_1 =$ | | 18 | k Ω |
| Resistor between screen grids and chassis | $R_2 =$ | | 27 | k Ω |
| Bias resistor | $R_b =$ | | 180 | Ω |
| Oscillator grid leak | $R_{gT+g3} =$ | | 22 | k Ω |
| Oscillator grid current | $I_{gT+g3} =$ | | 350 ¹⁾ | μ A |
| Grid bias | $V_{g1} =$ | | -2 — 27.5 | V |
| Screen grid voltage | $V_{g2+g4} =$ | | 85 | 119 V |
| Anode current | $I_a =$ | | 3.0 | — mA |
| Screen grid current | $I_{g2+g4} =$ | | 3.0 | — mA |
| Conversion conductance | $S_c =$ | | 750 | 7.5 μ A/V |
| Internal resistance | $R_i =$ | | >1 | >5 M Ω |
| Equivalent noise resistance | $R_{eq} =$ | | 100 | — k Ω |

Typical characteristics of the triode section (see Figs. 17 and 18)

| | | | |
|----------------------|-------------|---|----------|
| Anode voltage | V_a | = | 100 V |
| Grid voltage | V_{gT+g3} | = | 0 V |
| Anode current | I_a | = | 10 mA |
| Mutual conductance | S | = | 2.8 mA/V |
| Amplification factor | μ | = | 22 |

¹⁾ If the grid leak R_{gT+g3} equals 47 k Ω , the recommended value for I_{gT+g3} is 200 μ A for supply voltages of 200 and 170 V, and 100 μ A for a supply voltage of 100 V.

UCH 42

Operating characteristics of the triode section used as oscillator

(see Figs. 19 to 22 incl.)

| | | | | | | | | | |
|----------------------------|-------------|---|-----|-----|------|------------|------------|------|------|
| Supply voltage . . . | V_b | = | 100 | 170 | 200 | V | | | |
| Anode resistor . . . | R_a | = | 10 | 10 | 22 | k Ω | | | |
| Oscillator voltage . . . | V_{osc} | = | 4 | 8 | 8 | V_{RMS} | | | |
| Oscillator grid leak . . . | R_{gT+g3} | = | 22 | 47 | 22 | 47 | k Ω | | |
| Oscillator grid current | I_{gT+g3} | = | 175 | 100 | 350 | 200 | μ A | | |
| Anode current . . . | I_a | = | 3.4 | 3.1 | 6.5 | 5.7 | 5.5 | 5.2 | mA |
| Effective slope . . . | S_{eff} | = | 0.7 | 0.6 | 0.75 | 0.65 | 0.65 | 0.55 | mA/V |

Operating characteristics of the UCH 42 used as phase inverter

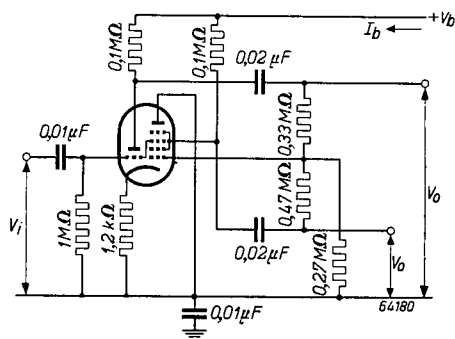


Fig. 4

| Supply voltage V_b (V) | Total current I_b (mA) | Amplification V_o/V_i | Distortion (%) at an output voltage of | |
|-----------------------------|-----------------------------|----------------------------|--|--------------|
| | | | 5 V_{RMS} | 10 V_{RMS} |
| 100 | 1.4 | 11 | 1.9 | — |
| 165 | 2.4 | 11 | 1.5 | 1.6 |

Operating characteristics of the hexode section used as frequency changer, together with that of the UAF 42, fed by means of a common potentiometer (see Figs. 23 to 25 incl.)

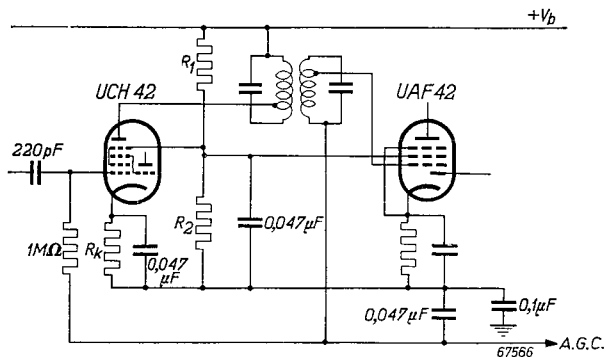


Fig. 5

| | | | | | |
|---|---------------|------------------------|-------------------|-----|---------|
| Anode and supply voltage | $V_a = V_b =$ | 100 | 170 | V | |
| Resistor between supply voltage and screen grids | $R_1 =$ | 15 | 15 | kΩ | |
| Resistor between screen grids and chassis | $R_2 =$ | 22 | 22 | kΩ | |
| Bias resistor | $R_k =$ | 180 | 180 | Ω | |
| Oscillator grid leak | $R_{gT+g3} =$ | 22 | 22 | kΩ | |
| Oscillator grid current | $I_{gT+g3} =$ | 175 ¹⁾ | 350 ¹⁾ | μA | |
| Grid bias | $V_{g1} =$ | -1.0 -9.6 -1.8 -15.5 V | | | |
| Screen grid voltage | $V_{g2} =$ | 43 | 58 | 70 | 99 V |
| Anode current | $I_a =$ | 1.2 | — | 2.1 | — mA |
| Screen grid current | $I_{g2+g4} =$ | 1.46 | — | 2.6 | — mA |
| Conversion conductance | $S_c =$ | 530 | 14 | 670 | 20 μA/V |
| Internal resistance | $R_i =$ | >1 | >2 | >1 | >4 MΩ |
| Equivalent noise resistance | $R_{eq} =$ | 60 | — | 66 | — kΩ |

Limiting values of the hexode section

| | | | |
|---|------------------------------------|--------|--------------------|
| Anode voltage, cut-off condition | V_{a_o} | = max. | 550 V |
| Anode voltage | V_a | = max. | 250 V |
| Anode dissipation | W_a | = max. | 1.5 W |
| Screen grid voltage, cut-off condition | $V_{(g2+g4)_c}$ | = max. | 550 V |
| Screen grid voltage, valve con- trolled | $V_{g2+g4}(I_a < 1\text{mA})$ | = max. | 250 V |
| Screen grid voltage, valve un- controlled | $V_{g2+g4}(I_a = 3\text{mA})$ | = max. | 125 V |
| Screen grid dissipation | W_{g2+g4} | = max. | 0.3 W |
| Grid current starting point | $V_{g1}(I_{g1} = +0.3\mu\text{A})$ | = max. | -1.3 V |
| Cathode current | I_k | = max. | 10 mA |
| External resistance between grid 1 and cathode | R_{g1} | = max. | 3 MΩ ²⁾ |
| External resistance between grid 3 and cathode | R_{g3} | = max. | 3 MΩ |
| External resistance between heater and cathode | R_{fk} | = max. | 20 kΩ |
| Voltage between heater and cathode | V_{jk} | = max. | 150 V |

¹⁾ See note on page 213.

²⁾ This value is applicable where the grid bias is derived from a cathode resistor.

UCH 42

Limiting values of the triode section

| | | | |
|--|------------------------------|--------|---------------|
| Anode voltage, cut-off condition | V_{a_c} | = max. | 550 V |
| Anode voltage | V_a | = max. | 175 V |
| Anode dissipation | W_a | = max. | 0.8 W |
| Grid current starting point | $V_g(I_g = +0.3\mu\text{A})$ | = max. | -1.3 V |
| Cathode current | I_k | = max. | 6 mA |
| External resistance between grid and cathode | R_g | = max. | 3 M Ω |
| External resistance between heater and cathode | R_{fk} | = max. | 20 k Ω |
| Voltage between heater and cathode | V_{fk} | = max. | 150 V |

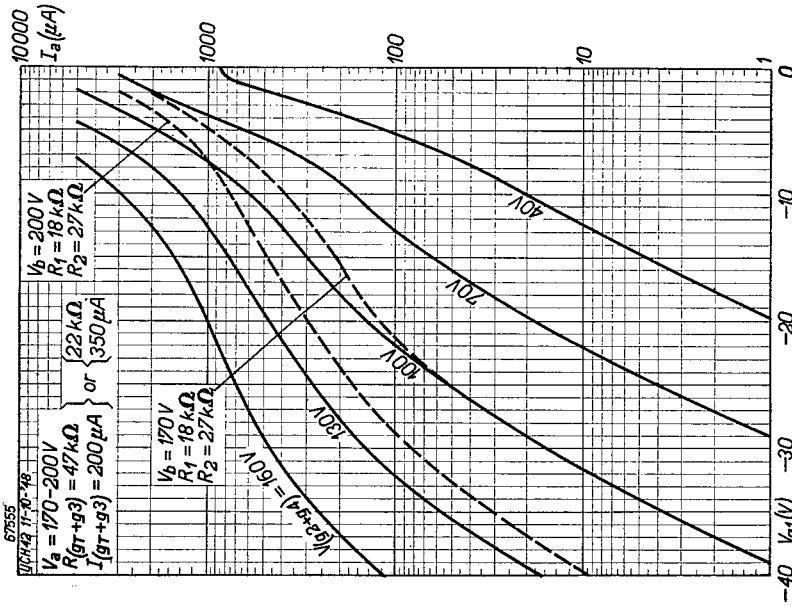


Fig. 7

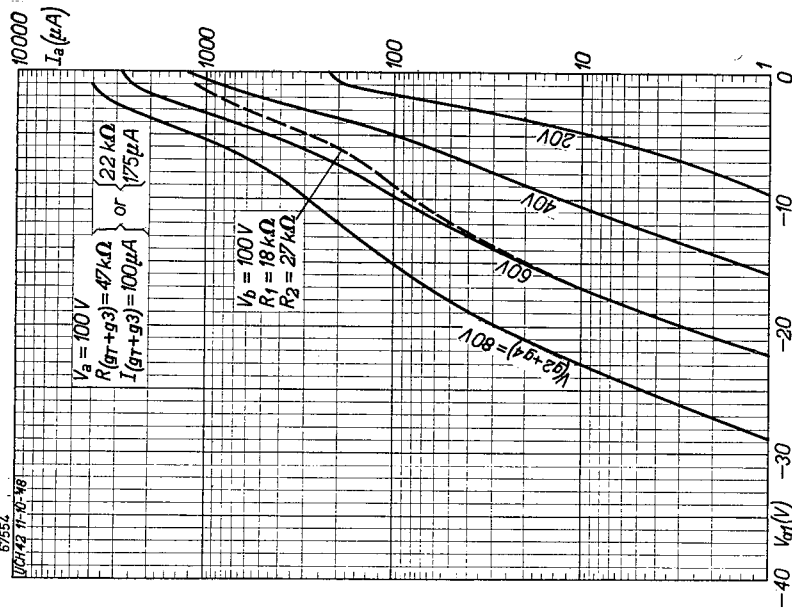


Fig. 6

Anode current (I_a) of the UCH 42 as a function of the grid bias (V_{g1}), measured on oscillating valve, with screen grid voltage (V_{g2+g4}) as parameter. The dotted lines represent the anode current when the screen grids are fed by means of a potentiometer (R_1, R_2 , see Fig. 3). Fig. 6: supply voltage $V_b = 100\text{ V}$; Fig. 7: $V_b = 170 - 200\text{ V}$.

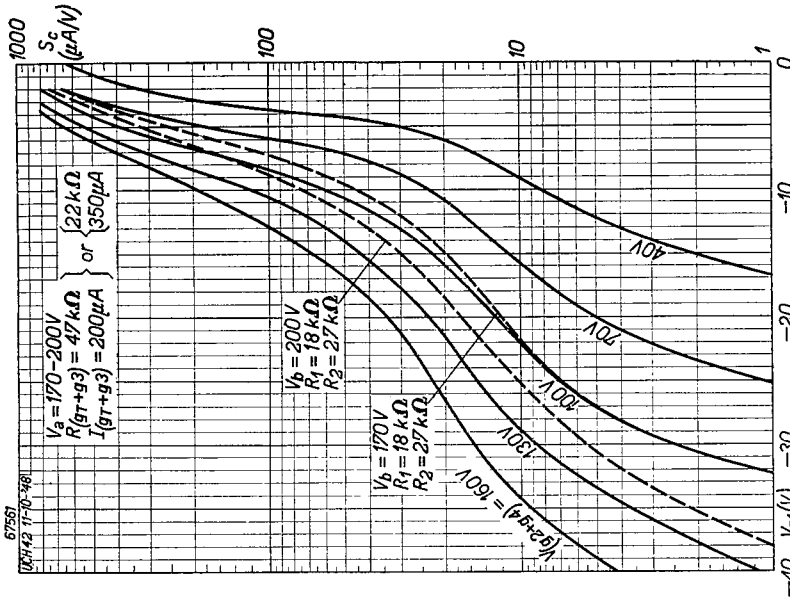


Fig. 9

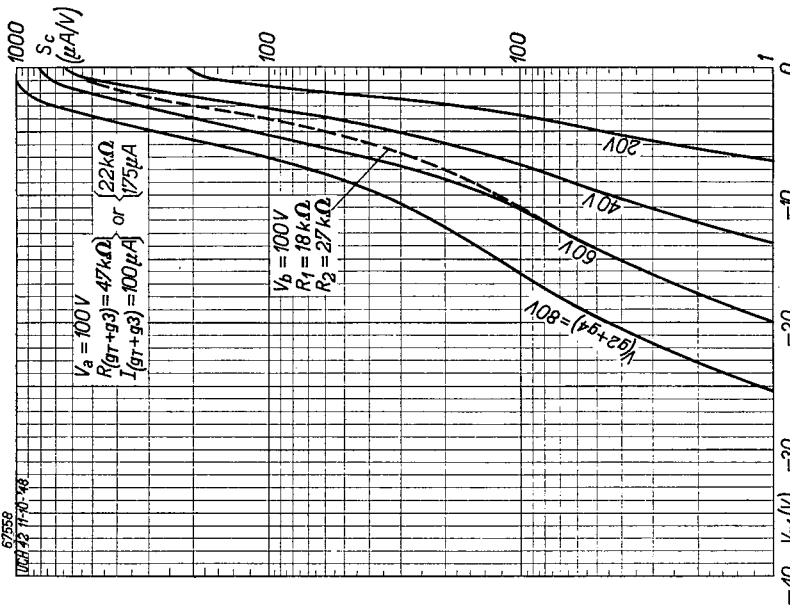


Fig. 8

Conversion conductance (S_c) of UCH 42 in oscillating condition, as a function of the grid bias (V_{g1}) with screen grid voltage (V_{g2+g4}) as parameter. The dotted lines indicate the conversion conductance when the screen grid voltage is derived from a potentiometer (R_1, R_2 in Fig. 3). Fig. 8 : supply voltage $V_b=100$ V ; Fig. 9 : $V_b=170 - 200$ V.

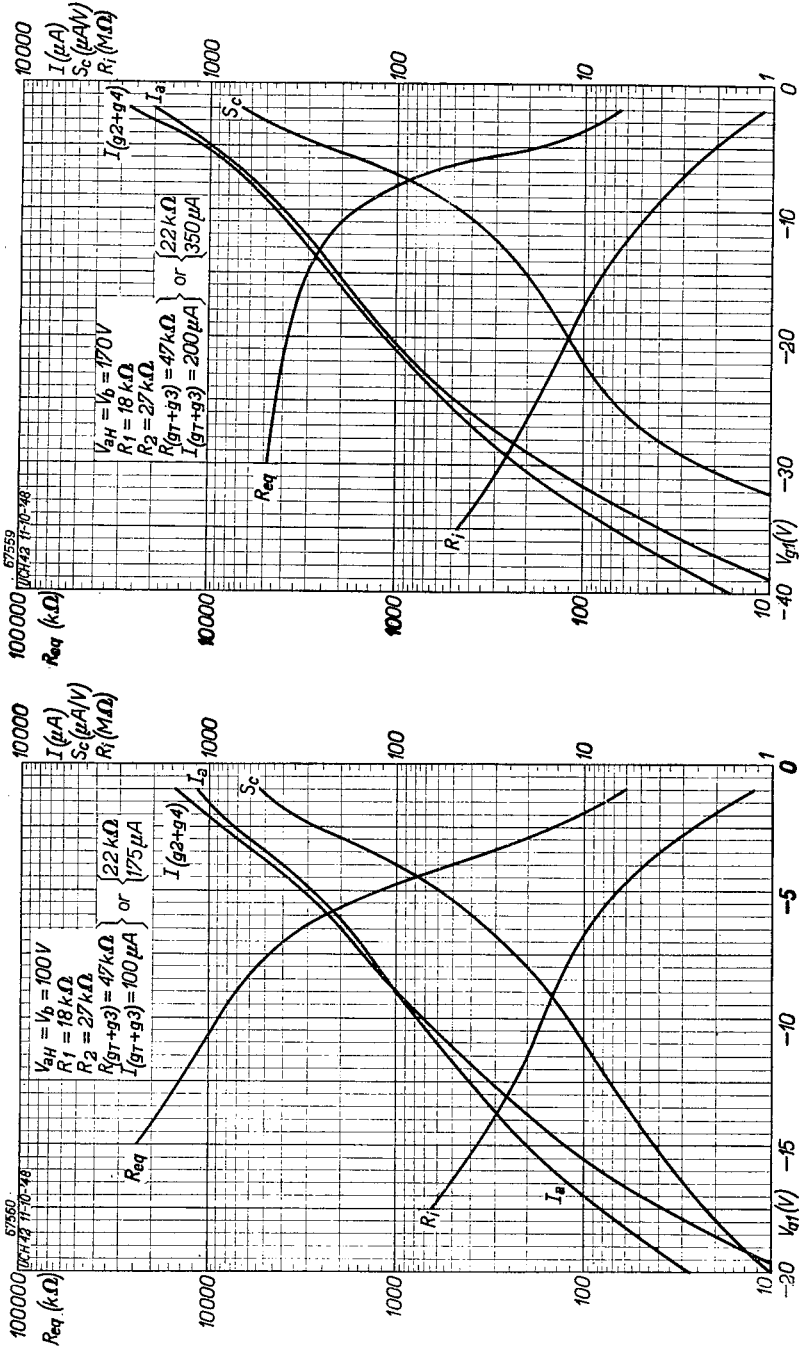


Fig. 10 Anode current (I_a), screen grid current (I_{g2+g4}), conversion conductance (S_c), internal resistance (R_i) and equivalent noise resistance (R_{eq}) of the UCH 42 in oscillating condition, as functions of the grid bias (V_{g1}). Measured in the circuit shown in Fig. 3. Fig. 10 : supply voltage $V_b = 100$ V. Fig. 11 : $V_b = 170$ V.

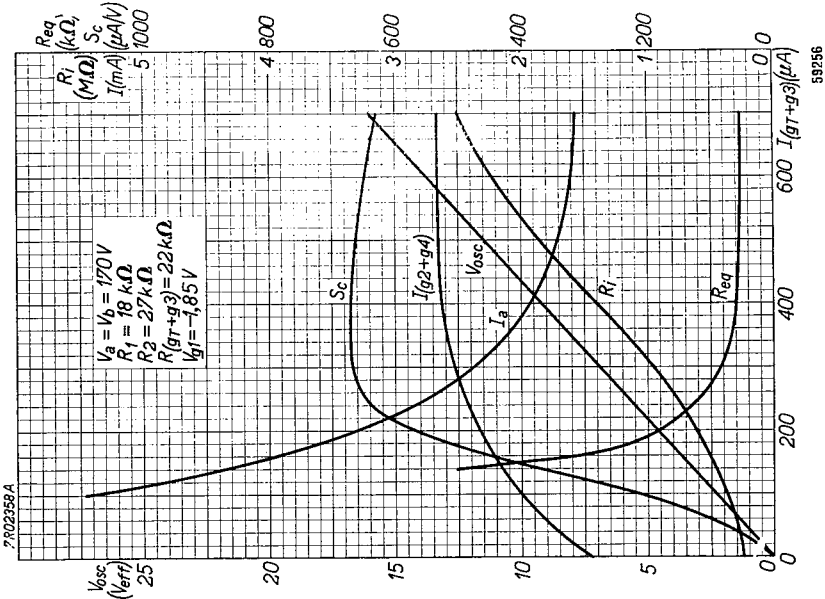


Fig. 13

oscillator voltage (V_{osc}), internal resistance (R_{eq}), anode current (I_a) and equivalent noise resistance (R_i) of the UCH 42 as functions of the oscillator grid current (I_{g1+g3}) for a grid leak R_{g1+g3} of 22 k Ω . Measured in the circuit shown in Fig. 3. Fig. 12 : supply voltage $V_b = 100\text{ V}$; Fig. 13 : $V_b = 170\text{ V}$.

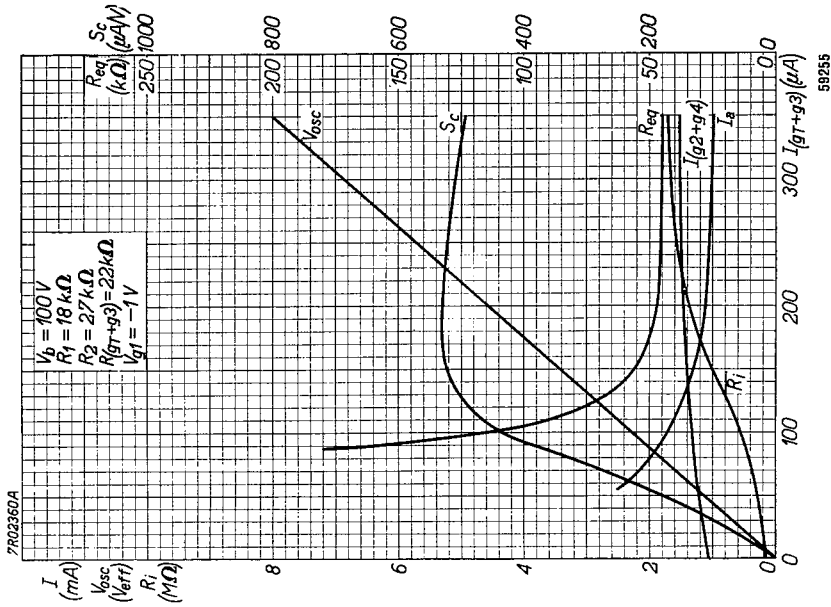


Fig. 12

Anode current (I_a), conversion conductance (S_c), oscillator voltage (V_{osc}), internal resistance (R_{eq}) and equivalent noise resistance (R_i) of the UCH 42 as functions of the oscillator grid current (I_{g1+g3}) for a grid leak R_{g1+g3} of 22 k Ω . Measured in the circuit shown in Fig. 3. Fig. 12 : supply voltage $V_b = 100\text{ V}$; Fig. 13 : $V_b = 170\text{ V}$.

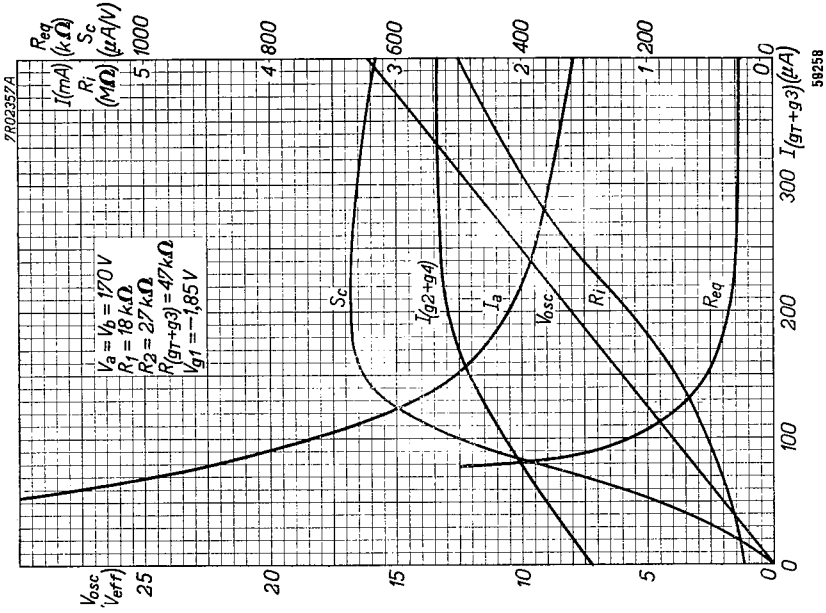


Fig. 15

As Figs. 12 and 13, but for grid leak R_{g1+g3} of $47 \text{ k}\Omega$.

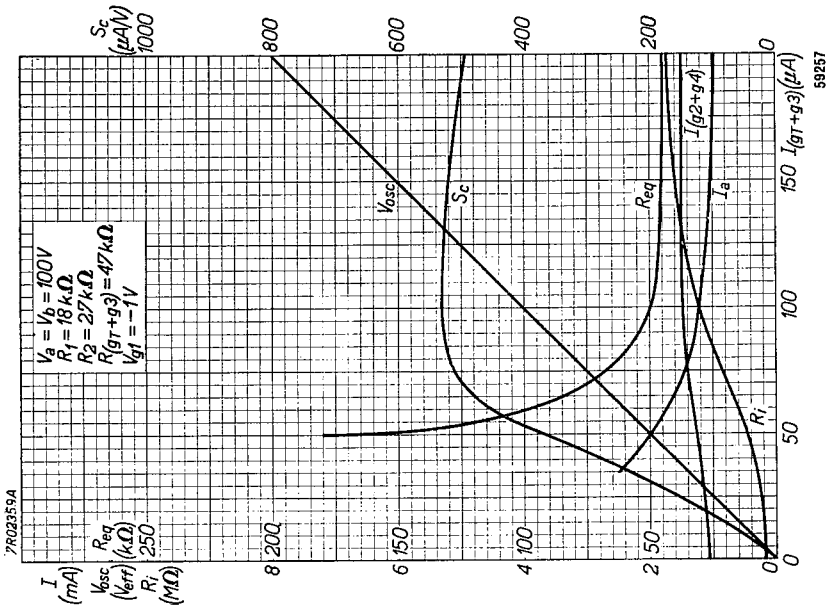


Fig. 14

As Figs. 12 and 13, but for grid leak R_{g1+g3} of $47 \text{ k}\Omega$.

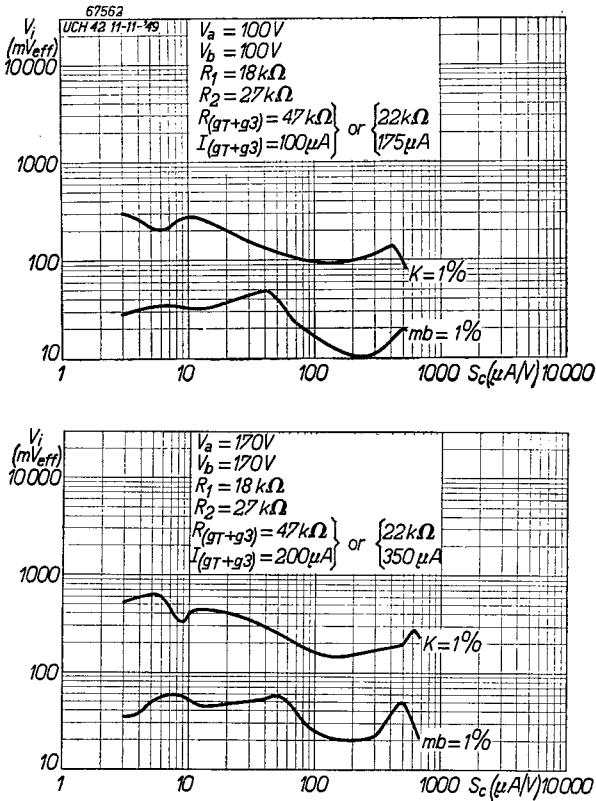


Fig. 16

- 1) The effective voltage (V_i) of an interfering signal at the control grid of the UCH 42 producing 1% cross modulation (curve $K=1\%$) and
- 2) the effective voltage (V_i) of a ripple signal at the control grid producing 1% modulation hum (curve $m_b=1\%$), both as function of the conversion conductance S_c and measured in the circuit shown in Fig. 3. Upper figure: supply voltage $V_b=100V$; lower figure: $V_b=170V$.

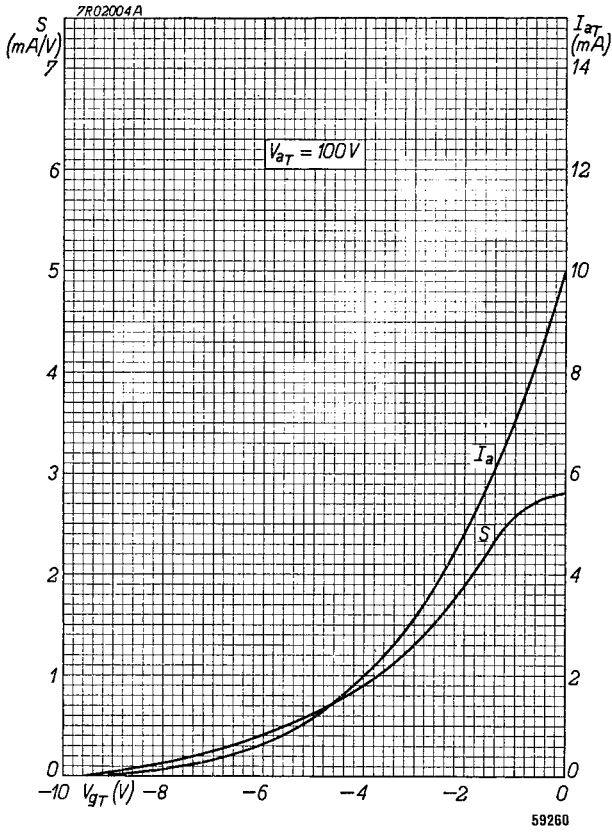
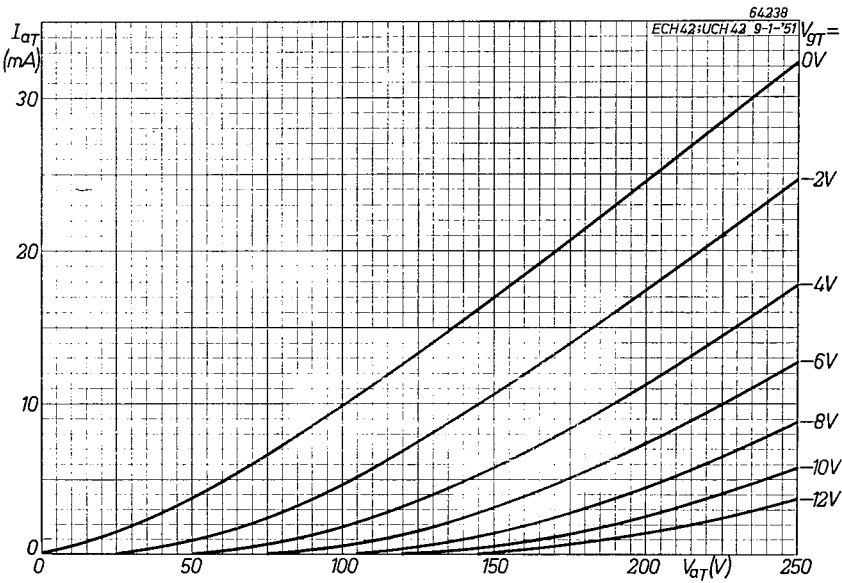


Fig. 17
 I_a/V_g and S/V_g characteristics of the triode section of the UCH 42.

Fig. 18
 I_a/V_a characteristics relative to the triode section of the UCH 42.



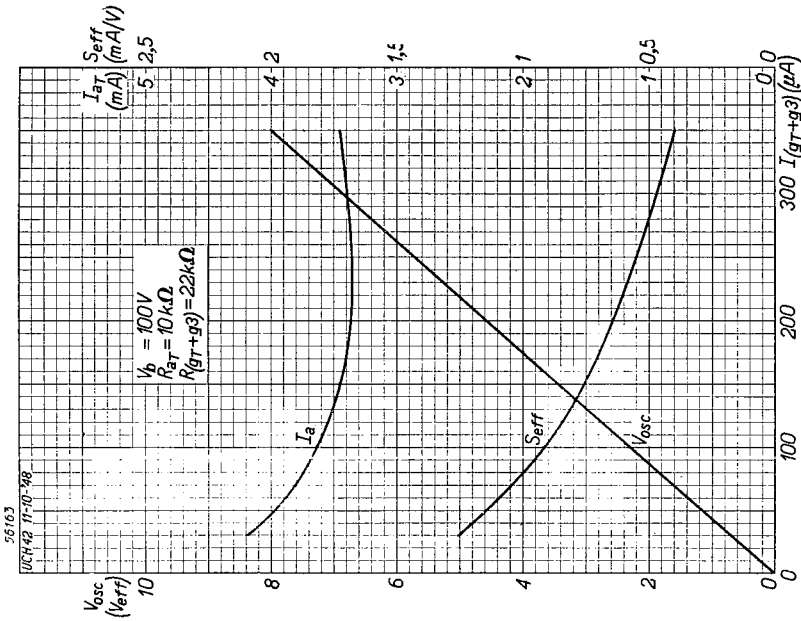


Fig. 19

Anode current (I_a), oscillator voltage (V_{osc}) and effective slope (S_{eff}) of the triode section of the UCH 42 as functions of the oscillator grid current (I_{gr+g3}), with grid leak (R_{gr+g3}) of 22 k Ω . Fig. 19: supply voltage $V_b=100$ V; Fig. 20: $V_b=170$ V.

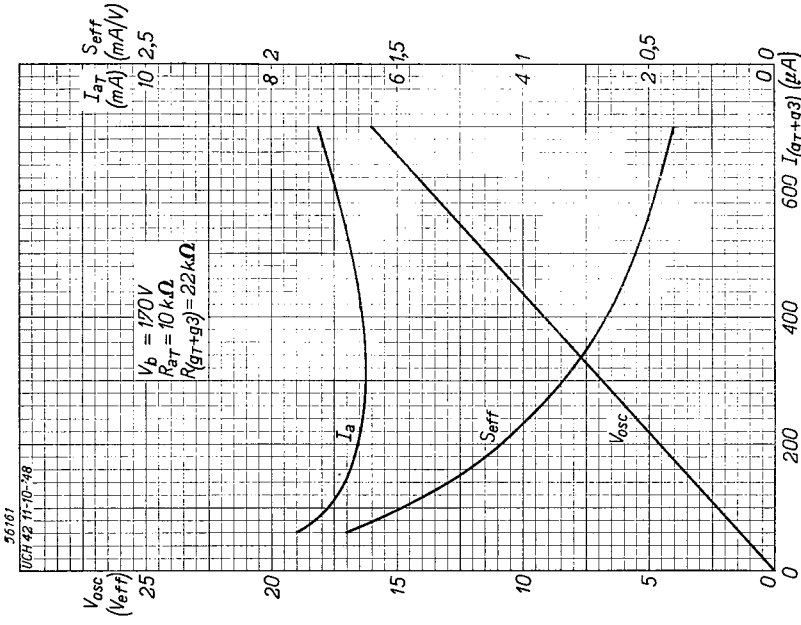


Fig. 20

Anode current (I_a), oscillator voltage (V_{osc}) and effective slope (S_{eff}) of the triode section of the UCH 42 as functions of the oscillator grid current (I_{gr+g3}), with grid leak (R_{gr+g3}) of 22 k Ω . Fig. 19: supply voltage $V_b=100$ V; Fig. 20: $V_b=170$ V.

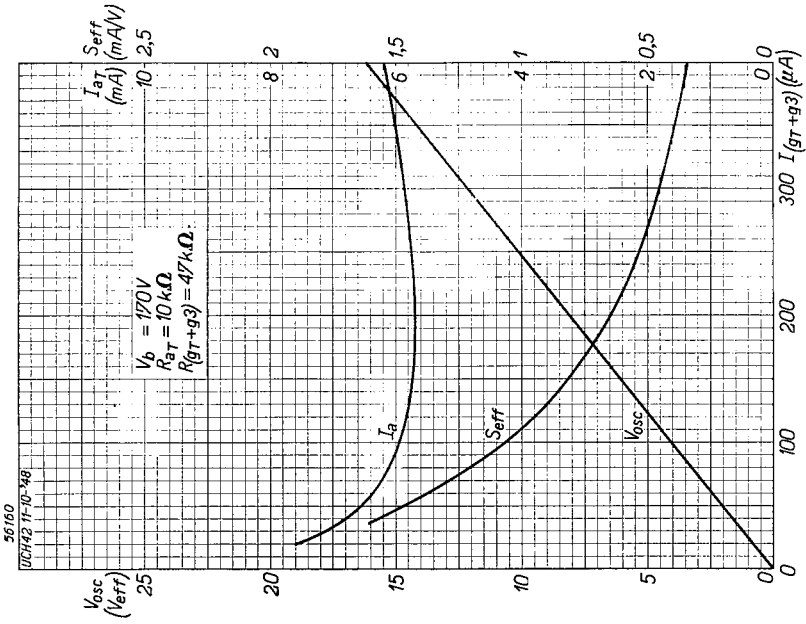


Fig. 22

As Figs. 19 and 20, but with a grid leak $R_{(gr+g3)}$ of 47 kΩ.

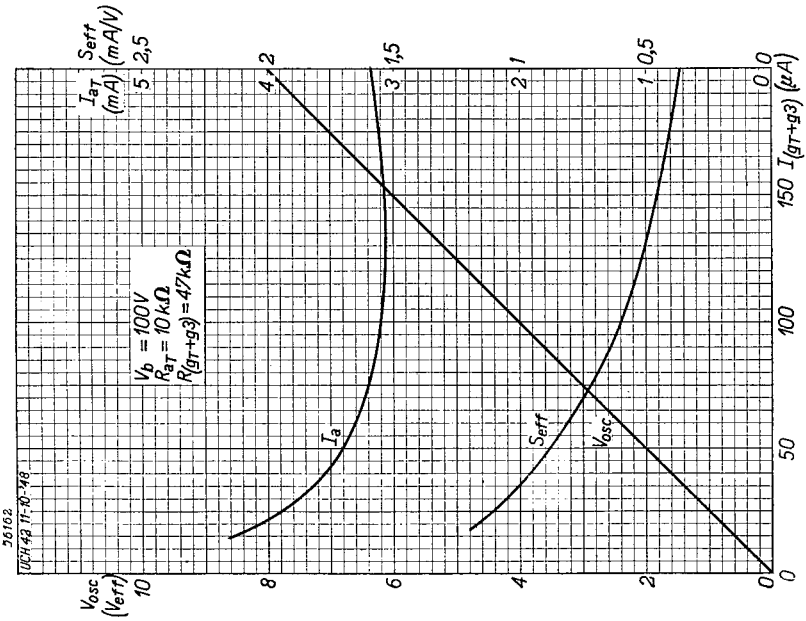


Fig. 21

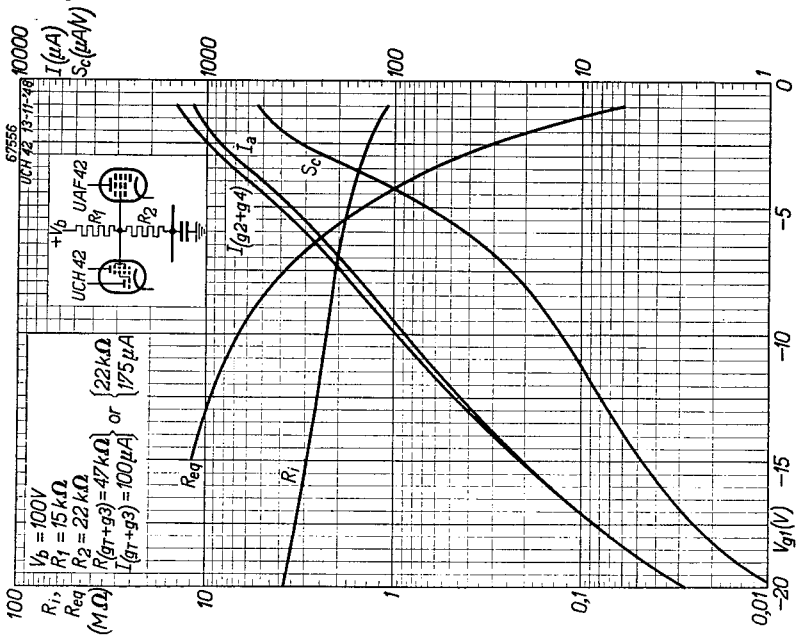
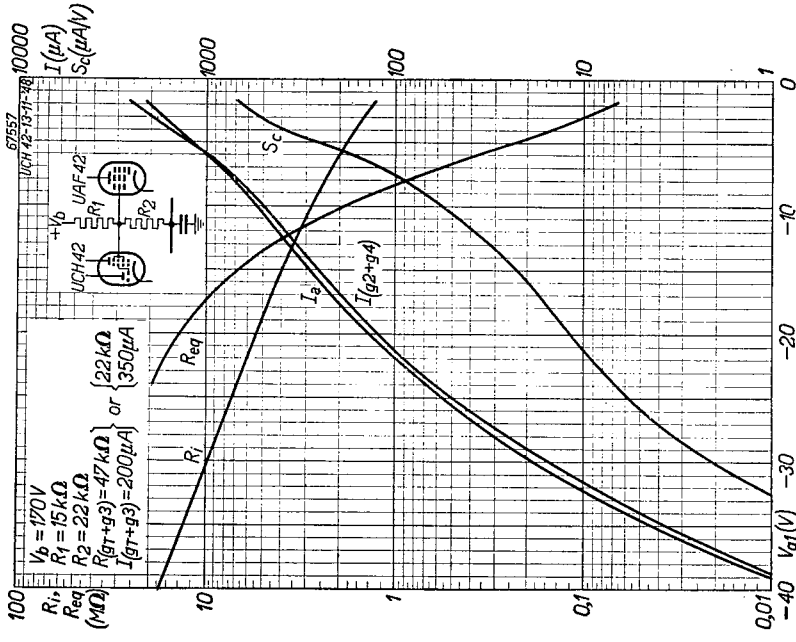


Fig. 23

As Figs. 10 and 11, but with the screen grid voltage of the UCH 42 together with that of the UAF 42 fed by means of a common potentiometer. Measured in the circuit shown in Fig. 5. Fig. 23 : supply voltage $V_b = 100 V$; Fig. 24 : $V_b = 170 V$.

Fig. 24



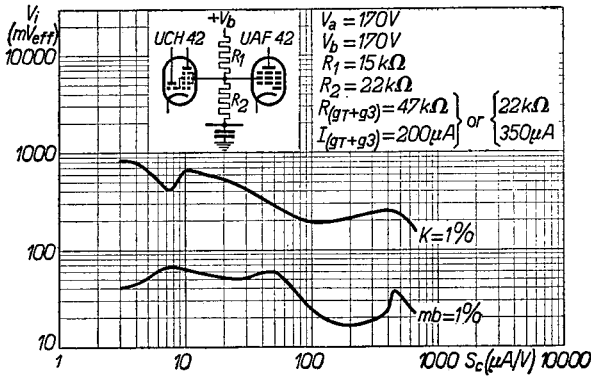
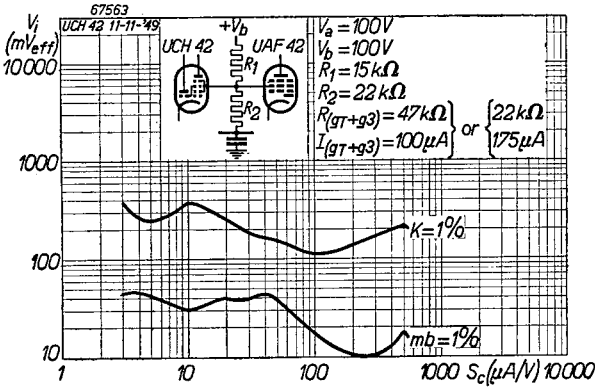


Fig. 25

As Fig. 16, but with the screen grids of the UAF 42 and UCH 42 fed by means of a common potentiometer.